RIDLEY WEBINAR SERIES: 9 CORE LOSS MODELING



Webinar November 12, 2020 10 am PDT Downloads: 9 Core Loss Modeling.pdf



Core Loss Modeling – the Players



Charles Proteus Steinmetz – great GE engineer working from the late 1890s.

Dr. Vatché Vorpérian – one of the best minds in our industry taught me about fractal mathematics.





Dr. Qichen Yang – solved complex mathematical problems for me involving 6th order circuit optimization. Dr. Shilpa Marti – spent 3 weeks reading and transcribing core loss data for us so that you don't have to do that anymore.





Arthur Nace – retired aerospace engineer and programmer who automated LTspice models for us. John Beecroft – Primary tester and proponent of RidleyWorks for over 20 years.



Semiconductor Devices and Models



These are impossibly complex structures to build and understand.

Yet they usually come with a spice model that's pretty useful.





Magnetics Devices and Models



Not so hard to build, although maybe hard to understand.

Doesn't compare to Schroedinger's equations.....

Where is the spice model





Magnetics Winding Loss Models









New Rac Model

Ridley Engineering Complex proximity loss models covered in this webinar



https://ridleyengineering.com/videos-e/304-magneticsproximity-loss-webinar.html

Core Loss MPP 200u

Core Loss Density Curves - MPP 200µ, 300µ



300 kHz 0.1 T 5 W/cm3



Core Loss PC95





300 kHz 0.1 T 0.350 W/cm3 > 10 times better than MPP



Steinmetz Equation

Material: PC95

$$P_c = kf^x \Delta B^y$$

Equation assumes curves are

- 1) Equally spaced with frequency
- 2) Equal slopes at different frequencies

Steinmetz Equation named for Charles Steinmetz, he introduced a form of this equation in **1892**. Core loss was a problem even at 50/60 Hz





Use Excel to Calculate Coefficients



Early Transformer Core Loss Model



Simple resistor captured some of the loss characteristics

Frequency was fixed to line distribution frequency (change resistor value for different frequency)

Hysteresis losses captured for sinewave excitation – flux exponent assumed to be 2



Parallel Ladder Network - Frequency Dependence

$$P_c = kf^x \Delta B^y$$



Parallel ladder driven by the inductor or transformer voltage

Frequency dependent dissipation matches frequency exponent

This will give a flux exponent of 2, like the early core loss models



Parallel Ladder Network – Adding y Exponent



Parallel ladder driven by the inductor or transformer voltage

Magnetic winding voltage is raised to the y/2 power

Waveform sign must stay the same



Data Entry and Model Generation

	ORMER CORE	MATERIAL SELE	CTION ——							
Ferroxcube		TDK		Magnetics	Any					
O 3C90	C 3C91	C PC40	O PC47	ОР	C MPP 200u	C New 11				
C 3F3	C New	C PC90	○ New	€ F	C New 8	C New 12	DATA	Core Material Loss Data		
© 3C96	○ New	C PC44	○ New	○ R	C New 9	O New 13		Core Manufacturer	Magnetic	Magnetics
		C PC95		○ New	C New 10	O New 14		Core Material	E	F
					Temperature	data used: 100 d	egrees C	Core Material		
CHARACTERISTICS FOR Permeability 3000		SELECTED MATE Magnetizing I	ATERIAL Ig Inductance 0.3311		Core Loss 0.4	176 W	1	60 Degrees C	Loss Data	(mW/cm3)
PSIM/LTSPICE CORE LOSS MODEL						Steinmetz	100 kHz 0.1 T	140	140	
Inductors	6 561 mH	104	22.544 mł	Resisto	20.13 0	RC5	138 66079 k0	100 kHz 0.2 T	760	760
LC2	9.907 mH	LC5	34.865 mF	H RC2	182.42 Ω	RC6	999.41181 kΩ	200 kHz 0.1 T	363	363
LC3	14.963 mH	2 538	41.882 mF	Steinmetz Coe	fficients	RC7	10.67 MΩ		New Value	Current Value
Volta	se exponent	2.000						100 Degrees C		
				Core N	1aterial		F	100 kHz 0.1 T	105	105
	(+)VPV			Core N	lanufacturer		Magnetics	100 kHz 0.2 T	610	610
	Ĭ	ຊີ LC1 ຊື] LC2] LC3					200 kHz 0.1 T	260	260
		_ ,	[]		$P_{core} = K\Delta$	$B^{x}f^{y}$	2			ок
							Steinmetz			
				Consta	int K		87.738			
	Flux exponent x					2.538				
	Frequency Exponent y					1.308				

Ridley Engineering

Fully Automated PSIM and LTspice Models



Transformer Core Loss Model

.param CLexp=2.160964 .param Rc1=40705.33 .param Rc2=139656.09 .param Rc3=479205.38 .param Rc4=1640976.57 .param Rc5=5814347.47 .param Rc6=12931115.75 .param Rc7=117724615.34 .param Lc1=7.600474 .param Lc2=4.346083 .param Lc3=2.48547 .param Lc4=1.418528 .param Lc5=0.837693 .param Lc6=0.310505 .param Coupling=0.007820



LTspice Simulation Results



High Line Input



Hands-On Design Workshops



January 25-28, February 22-25

This is our brand-new workshop format where we ship you everything you need to design, test, and learn. Magnetics kits with cores, bobbins and wire, custom computer and software, oscilloscope, frequency response analyzer, power supplies, load banks, test boards and parts kits are included. It's a learning experience like no other where we teach real-time and monitor each of your individual test stations from our base in California.

All attendees receive course notes and their personal copy of RidleyWorks to greatly accelerate your design process.





Email <u>info@ridleyengineering.com</u> For full demo

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Frequency Response Analyzers

Power Supply Design Center Facebook Group





Power Supply Design Center Articles









Power Stage Designer Power Stage Waveforms Magnetics Designer Transfer Function Bode Plots Closed Loop Design Automated FRA Control LTspice® Automated Link PSIM® Automated Link



4-Channel Frequency Response Analyzer

Frequency Range 1 Hz - 20 MHZ Source Control from 1 mV - 4 V P-P Built-In Injection Isolator Bandwidth 1 Hz - 1 kHz Automated Setup from RidleyWorks® Drect Data Flow into RidleyWorks®



4-Channel 200 MHz Oscilloscope

Picoscope[®] 5444D 4-Channel Oscilloscope 200 MHz Bandwidth 1 GS/s at 8-bit res; 62.5 MS/s at 16-bit res Signal Generator up to 20 MHZ Computer Controlled



Ridley Engineering

Embedded Computer

Intel[®] Computer with 32 GB RAM, 256 GB SSD Intel[®] HD Graphics 620 Integrated Dual Band Wireless, Bluetooth 4.2 Dual HDMI and USB Ports, Ethernet

