Course 1: How to solve circuits the right way – once and for all!

Lecture 1

The Joys of Circuit Analysis

Course 1: How to solve circuits the right way – once and for all!

Based on my book:

"Fast Analytical Techniques in Electrical and Electronic Circuits" Published by Cambridge University Press, 2002. **Course 1**: How to solve circuits the right way – once and for all!

Lecture 1

- 1. Meaningful and meaningless solutions to circuits.
- 2. Painful circuit analysis.
- 3. Painless and joyful circuit analysis.
- 4. Excruciating circuit analysis.
- 5. More joyful circuit analysis.
- 6. Dr. R.D. Middlebrooks's Legacy.

Excruciating circuit analysis

Example 1: Extract g_m as a parameter in the input resistance of the bridge circuit with a dependent trans-conductance source, $g_m v_1$, shown in the figure.

This means that the input resistance should be in the form:

$$R_{in} = \frac{A + Bg_m}{C + Dg_m}$$

In which A, B, C and D are not functions of g_m .



Excruciating circuit analysis

Example 1: (cont.)

I do not expect you to follow the next sixteen steps of algebraic misery to perform the method of parameter extraction using the nodal equations of this circuit.

This excruciating method is described in the following well-known reference:

L.O.Chua and Pen-Min Lin, *Computer Aided Analysis of Electronic Circuits: Algorithms and Computational Techniques*, Prentice Hall, New York, 1975.

I am including it in my lectures *only to drive home harder the concept of painless circuit analysis* that I am teaching.



 \mathbf{g}_2

6

RB

 $g_m v$

 $g_3 \ge$

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Excruciating circuit analysis

Example 1: (cont.)

STEP 1: Determine the Indefinite Admittance Matrix by *adding* a new element $R_s = 1/g_s$ at the input port! **From the first step, you can already see that this is NOT**

g_s <

going in the right direction!

Instead of simplifying the circuit, you are making it more complex!

Nevertheless let us proceed!

Label the nodes and the sources V_1 through V_4 .

Write the nodal equations and the IAM as follows:

 $I = Y_{ind}V$

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Excruciating circuit analysis

Example 1: (cont.)

STEP 2: At each node *n*, determine the current I_n using superposition for V_1 through V_4 and obtain:

$$Y_{ind} = \begin{bmatrix} g_1 + g_2 + g_s & -g_2 & -g_1 & -g_s \\ g_m - g_2 & g_2 + g_B + g_4 & -g_m - g_B & -g_4 \\ -g_m - g_1 & -g_B & g_m + g_B + g_1 + g_3 & -g_3 \\ -g_s & -g_4 & -g_3 & g_s + g_3 + g_4 \end{bmatrix}$$

This was not bad because all we had to do was write simple equations and use superposition.

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Excruciating circuit analysis

Example 1: (cont.)

STEP 3: Extract g_s according to the following cofactor theorem.

Theorem. If a parameter, α , appears as $(+\alpha)$ in positions (i,k) and (j,m) and as $(-\alpha)$ in positions (i,m) and (j,k) in the indefinite admittance matrix Y_{ind} , then:

Cofactor of $Y_{ind} = \text{Cofactor of } Y_{ind} \Big|_{\alpha=0} + (-1)^{j+m} \alpha \text{ Cofactor of } (Y_{\alpha})$

where Y_{α} is another indefinite admittance matrix not containing α and obtained from Y_{ind} as follows:

- 1. Add row j to row i in Y_{ind} .
- 2. Add column m to column k in Y_{ind} .
- 3. Delete row j and column m in Y_{ind} .

Note: ALL cofactors of an IAM are equal.

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Excruciating circuit analysis

Example 1: (cont.)

In our case $\alpha = g_s$ so that we have:

Cofactor of $Y_{ind} = \text{Cofactor of } Y_{ind} \Big|_{g_s=0} + (-1)^{j+m} g_s \text{ Cofactor of } (Y_{g_s})$

STEP 4: Determine $Y_{ind}\Big|_{g_s=0}$

$$Y_{ind}\Big|_{g_s=0} = \begin{bmatrix} g_1 + g_2 & -g_2 & -g_1 & 0 \\ g_m - g_2 & g_2 + g_B + g_4 & -g_m - g_B & -g_4 \\ -g_m - g_1 & -g_B & g_m + g_B + g_1 + g_3 & -g_3 \\ 0 & -g_4 & -g_3 & g_3 + g_4 \end{bmatrix}$$

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Example 1: (cont.)

STEP 5: Determine Y_{g_s}

$$Y_{g_s} = \begin{bmatrix} g_1 + g_2 + g_3 + g_4 & -g_2 - g_4 & -g_1 - g_3 \\ g_m - g_2 - g_4 & g_2 + g_B + g_4 & -g_m - g_B \\ -g_m - g_1 - g_3 & -g_B & g_m + g_B + g_1 + g_3 \end{bmatrix}$$

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Excruciating circuit analysis

Example 1: (cont.)

STEP 6: Extract g_m from $Y_{ind}\Big|_{g=0}$ by a *second* application of the cofactor theorem Cofactor of $Y_{ind}\Big|_{g_s=0} = \text{Cofactor of } Y_{ind}\Big|_{g_s=0} + (-1)^{j+m} g_m \text{ Cofactor of } (Y_{ind}\Big|_{g_s=0})$ **STEP 7:** Determine $Y_{ind}|_{g_s=0}$ $g_m = 0$ $Y_{ind} \Big|_{\substack{g_s=0\\g_m=0}} = \begin{bmatrix} g_1 + g_2 & -g_2 & -g_1 & 0\\ -g_2 & g_2 + g_B + g_4 & -g_B & -g_4\\ -g_1 & -g_B & g_B + g_1 + g_3 & -g_3\\ 0 & -g_4 & -g_3 & g_3 + g_4 \end{bmatrix}$

Excruciating circuit analysis

Example 1: (cont.)

STEP 8: Determine
$$Y_{ind} \Big|_{\substack{g_s = 0 \\ g_m}}$$

 $+g_m$ occurs in the positions (2,1) and (3,3) and $-g_m$ occurs in positions (3,1) and (2,3).

$$Y_{ind}\Big|_{g_s=0} = \begin{bmatrix} g_2 & -g_2 & 0\\ g_3 - g_2 & g_2 + g_4 & -g_3 - g_4\\ -g_3 & -g_4 & g_3 + g_4 \end{bmatrix}$$

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Example 1: (cont.)

STEP 9: Extract g_m from Y_{g_s} by a second application of the cofactor theorem

Cofactor of
$$Y_{g_s} = \text{Cofactor of } Y_{g_s} \Big|_{g_m=0} + (-1)^{j+m} g_m \text{ Cofactor of } (Y_{g_s,g_m})$$

STEP 10: Determine $Y_{g_s}\Big|_{g_m=0}$

$$Y_{g_s}\Big|_{g_m=0} = \begin{bmatrix} g_1 + g_2 & -g_2 - g_4 & -g_1 - g_3 \\ -g_2 - g_4 & g_2 + g_B + g_4 & -g_B \\ -g_1 - g_3 & -g_B & g_B + g_1 + g_3 \end{bmatrix}$$

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Example 1: (cont.)

STEP 11: Determine Y_{g_s,g_m}

 $+g_m$ occurs in the positions (2,1) and (3,3) and $-g_m$ occurs in positions (3,1) and (2,3) in Y_{α}

$$Y_{g_s,g_m} = \begin{bmatrix} g_2 + g_4 & -g_2 - g_4 \\ -g_2 - g_4 & g_2 + g_4 \end{bmatrix}$$

Excruciating circuit analysis

Example 1: (cont.)

STEP 12: Determine the cofactor
$$Y_{ind} \Big|_{\substack{g_s=0\\g_m=0}}$$

Since all cofactors are the same, we chose the simplest possible which is the following determinant:

Cofactor of
$$Y_{ind}\Big|_{\substack{g_s=0\\g_m=0}} = \begin{vmatrix} g_1 + g_2 & -g_2 & 0\\ -g_2 & g_2 + g_B + g_4 & -g_4\\ 0 & -g_4 & g_3 + g_4 \end{vmatrix}$$

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Excruciating circuit analysis

Example 1: (cont.) **STEP13:** Determine the cofactor $Y_{ind} \Big|_{\substack{g_s=0\\g_m}}$ Cofactor of $Y_{ind} \begin{vmatrix} g_s = 0 \\ g_m \end{vmatrix} = \begin{vmatrix} g_2 & 0 \\ -g_3 & g_3 + g_4 \end{vmatrix}$ **Step 14:** Determine the cofactor $Y_{g_s}\Big|_{g_m=0}$ Cofactor of $Y_{g_s}|_{g_m=0} = \begin{vmatrix} g_2 + g_B + g_4 & -g_B \\ -g_B & g_B + g_1 + g_3 \end{vmatrix}$

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Example 1: (cont.)

STEP 15: Determine the cofactor Y_{g_s,g_m}

Cofactor of
$$Y_{g_s,g_m} = g_2 + g_4$$

STEP 16: From the relationship between the Indefinite Admittance Matrix and Admittance Matrix one can show that:

$$Z_{in} = \frac{\operatorname{Cof.} Y_{g_s} \Big|_{g_m = 0} + g_m \operatorname{Cof.} Y_{g_s, g_m}}{\operatorname{Cof.} Y_{ind} \Big|_{\substack{g_s = 0 \\ g_m = 0}} + g_m \operatorname{Cof.} Y_{ind} \Big|_{\substack{g_s = 0 \\ g_m}}$$

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DISCUSSION:

- 1. The method of parameter extraction is about as painful as tooth extraction without $N_2O!$
- 2. You arrive at the answer after you expand four determinants assuming you have survived the algebra.
- 3. This is exactly how you get meaningless solutions to network problems.
- 4. This is exactly how you get turned off from electronic circuits.
- 5. This is how you put yourself at the mercy of circuit simulation programs trying to make sense out of a circuit.

Vorpérian Lecture Series Vorpérian Lecture Series **Vorpérian Lecture Series** Episode 3 Episode 1 Episode 2 Painful analysis of a simple bridge circuit R,a,)R,r. Painless circuit analysis $(R_1 + r_m)(R_1r_2 + R_2(r_2 + R_1))$ **Complete Vorperian** rat resistance, you solve for V₁ in terms of the using Cramer's rule: Multiple meaningful solutions: For example if we take R, out then we have the for OVin gain above obtained in meaningful form; $|G_1 + G_2 + G_3|$ $-G_D$ $G_Z + G_L + G_H$ **Lecture Notes** $-G_B$ $\begin{array}{c} -G_2 \\ -G_9 \\ G_2 + G_4 + G_9 \end{array}$ $1 - \frac{r_n}{a_n R_n}$ - $\begin{array}{c} \mathbf{s}_{2} & \mathbf{s}_{2} + \mathbf{G}_{4} + \mathbf{G}_{6} \end{bmatrix} \\ \mathbf{s}_{1} \text{ for a new install obtains. The the one was get for the strong non-transfer the strong non-transfer as problems. The strong non-transfer as a problem is a strong non-transfer to a strong non-transfer as a strong non-transfer to a st$ 1@#IT MOPR $= \bigvee_{1+R_2} \frac{1}{R_2 + R_2 ||r_c|}$ $R_1 \parallel r_{m}$ Vorpérian Power Electronics Engineering Vorpérian Power Electronics Engineering Vorpérian Power Electronics Engineering LLC CONVERTER DESIGN USING MAGNETICS CORE LOSS WEBINAR HAPPY HOUR WITH DR. RIDLEY DESIGN, BUILD AND TEST A SCALING LAWS WEBINAR FLYBACK TRANSFORMER WEBINAR This unique presentation is by our In this groundbreaking webinar, Dr. This is an open discussion without In this webinar Dr. Ridley shows you Ridley demonstrates circuit models for guest speaker Nicola Rosano. The any formal presentation from Dr. how to Design, Build, and Test a Flyback Transformer. We had the complex process of LLC converter core loss that provide loss estimations Ridley. Ask any questions you like design becomes very straightforward regardless of waveform. The models about power electronics, history, ambitious plan to actually build the **Ridley Webinar** with the application of standardized provide better worst-case analysis frequency response, topologies, transformer live during the webinar. curves combined with power and than the original data technology, people, or the past and **Series** frequency scaling concepts. future of our field. RIDLEY WEBINAR SERIES: 9 RIDLEY WEBINAR SERIES: 7 **RIDLEY WEBINAR SERIES: 8** DLEY WEBINAR SERIES: FLYBACK TRANSFORMER DESIGN CAREERS CORE LOSS JOBS, AND MODELING RESEARCH



Frequency Response Analyzers





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